

Receiver Saturation Point

Given the gain G_{RX} of a receiver, we know that the output signal power (i.e., the signal power at the demodulator) is:

$$P_D^{in} = P_s^{out} = G_{RX} P_s^{in}$$

Of course, P_s^{in} can theoretically be any value; but P_s^{out} is limited!

Q: Limited by what?

A: Many of the devices in a receiver have compression points (e.g., mixers and amplifiers)!

In other words, as P_s^{in} increases, one of the devices in the receiver will eventually compress (i.e., saturate). As we increase the signal power P_s^{in} beyond this point, we find that the receiver output power will be less than the value $G_{RX} P_s^{in}$.

→ Precisely the same behavior as an amplifier or mixer!

Accordingly, we can define a 1dB compression point for our receiver.

We can **approximately** determine the compression point of our receiver if we know **both** the gain (attenuation) and compression point of each and **every** one of its components.

Q: This sounds **very** much like how we determined the overall noise figure of a receiver (i.e., with knowledge of G and F for **every** component). Give me the equivalent **equation** so I can get busy calculating the compression point of my receiver!

A: Not so fast! The procedure for determining the compression point of a receiver is quite a bit **more complex** than finding its noise figure.

The problem is that the compression point of a receiver is not some function of the **all** the compression points of each device. Instead, it is dependent **only** on the compression point of the device that saturates first as P_s^{in} increases.

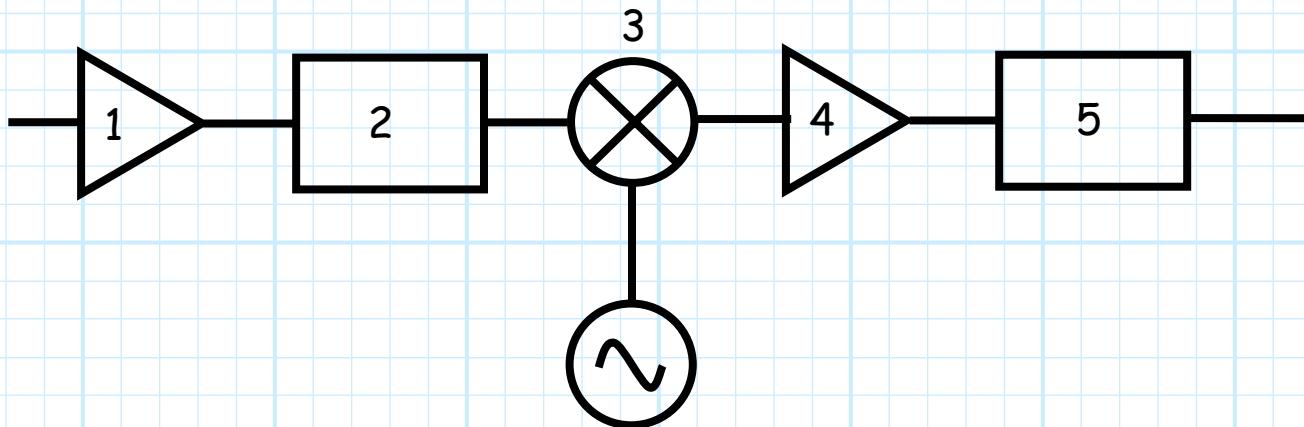
Big problem → we do **not** know what device will saturate first!

Q: Won't it simply be the device with the **lowest** 1 dB compression point?

A: **Nope!** The gain (or attenuation) of all of the devices that precede a component will likewise determine the value of receiver input power P_s^{in} at which that component saturates.

Thus, we must individually determine the value of receiver input power P_s^{in} that will cause each of the components in our receiver to saturate. The **smallest** of these values will be the compression point of the receiver!

Perhaps this is best explained by an example. Consider a simple super-het receiver with the following components:



Device	G_m	P_m^{1dB}	P_{in}^{sat}
$m=1$	10 dB	+10 dBm	
$m=2$	-1.0 dB	∞	
$m=3$	-6.0 dB	3 dBm	
$m=4$	15 dB	+14 dBm	
$m=5$	-2 dB	∞	

Here the value G_m represents the gain of the m -th component, P_m^{1dB} the 1dB compression point of the m -th component, and P_{in}^{sat} is the amount of receiver input power required to cause that particular component to saturate.

Now, let's look at **each** component, and determine its **particular** value for P_{in}^{sat} .

$m=1$: LNA

Recall the 1 dB compression point of an amplifier is specified in terms of **output** power. Thus, when this amplifier saturates, the **input** power will be:

$$P_{in1}^{1dB} = \frac{P_1^{1dB}}{G_1}$$

or equivalently:

$$\begin{aligned} P_{in1}^{1dB} (\text{dBm}) &= P_1^{1dB} (\text{dBm}) - G_1 (\text{dB}) \\ &= 10 - 10 \\ &= 0 \text{ dBm} \end{aligned}$$

Q: Wait! Shouldn't we add 1 dBm to this answer??

A: Theoretically yes, as when the device has compressed by 1 dB, the gain is effectively 1 dB less (i.e., $G_1 = 9\text{dB}$). However, we typically do **not** consider this fact when computing compression point, as:

1. 1 dBm is generally not large enough to be **numerically significant**, particularly when considering all the other approximations and **uncertainties** in our design!
2. By not adding the 1 dBm to the solution, we have a bit more **conservative** estimate of receiver performance. After all, our goal is to **avoid** receiver saturation!

Now, since the input to the LNA is likewise the input to the **receiver**, we can conclude that the LNA will saturate when the receiver input power is 0 dBm. Thus, "according to" our first component:

$$P_{in}^{sat} = 0 \text{ dBm}$$

However, this very well may **not** be the input value at which the receiver saturates, as some **other** component may compress at an even **lower** receiver input power.

→ Let's find out if there is such a component!

m=2: Preselector Filter

Q: Wait a second! I don't recall ever hearing about a **filter compression point**!?

A: True enough! A filter, since it is a **passive** and **linear** device, has **no** compression point. Of course, if we put too much power into the device, it will damage (e.g. melt) it, but this power is typically **very large** compared to most amplifier or mixer compression points.

Thus, we can conclude that the compression point of a filter is **effectively infinity**, as is the input receiver power required to "saturate" it (i.e., $P_{in}^{sat} = \infty$).

Q: *I see! Filters make no difference in determining the saturation point of a receiver. Can we ignore them altogether?*

A: *Absolutely not! Although filters will not saturate, they will help determine the saturation point of a receiver.*

The reason is that filters have **insertion loss**. Note the gain of this filter is -1.0 dB, which indicates an insertion loss of +1.0 dB. This loss will affect the input power of all the components further down the receiver "chain", and thus may affect the receive saturation point!

m=3: Mixer



Don't forget that the 1dB compression point of a mixer (unlike an amplifier) is specified in terms of its **input power**!

Thus, from the mixer compression point, we can **immediately** conclude that:

$$P_{in3}^{1dB} (dBm) = P_3^{1dB} (dBm) = 3 dBm$$

In other words, we do **not** have to "remove" the mixer conversion loss to find the input power, the way we had to

subtract the LNA gain from the LNA (output) compression point.

However, since the mixer is not directly connected to the input of the receiver, we must "remove" the gain of the preceding components in order to determine what **input receiver power** will cause the mixer to saturate.

Since the power into the mixer is simply the power into the receiver times the gain of the LNA and preselector filter:

$$P_{in3} = P_{in} G_1 G_2$$

we can conclude that:

$$P_{in}^{sat} = \frac{P_{in3}^{sat}}{G_1 G_2}$$

or equivalently:

$$\begin{aligned} P_{in}^{sat} (dBm) &= P_{in3}^{sat} (dBm) - G_1 (dB) - G_2 (dB) \\ &= 3 - 10 - (-1) \\ &= -6.0 dBm \end{aligned}$$

Note here that the 1dB insertion loss (i.e., $G_2 = -1.0 \text{ dB}$) of the **filter** was involved in our computation, and thus affected the value of this saturation point!

m=4: IF Amp

This IF amplifier saturates when its **output** power is $P_4^{1dB} = +14 \text{ dBm}$. The **receiver** input power that would cause this much output power at our **IF amp** can be (approximately) determined by "removing" the gain of each preceding device, including the gain of the amplifier itself (do you see why?):

$$\begin{aligned} P_{in}^{sat} (\text{dBm}) &= P_4^{1dB} (\text{dBm}) - G_4 (\text{dB}) - G_3 (\text{dB}) - G_2 (\text{dB}) - G_1 (\text{dB}) \\ &= 14 - 15 - (-6) - (-1) - 10 \\ &= -4 \text{ dBm} \end{aligned}$$

Note that the **gain** of the mixer is -6 dB; meaning that the **mixer conversion loss** is +6 dB.

It is now evident that we can write a **general equation** for determining the input receiver power that will cause an **amplifier** to saturate, when that amp is the m -th component of a receiver:

$$\begin{aligned} P_{in}^{sat} (\text{dBm}) &= P_m^{1dB} (\text{dBm}) - G_m (\text{dB}) - G_{m-1} (\text{dB}) - \dots - G_1 (\text{dB}) \\ &= P_m^{1dB} (\text{dBm}) - \sum_{n=1}^m G_n (\text{dB}) \quad (\text{for amplifiers}) \end{aligned}$$

Note the expression for **mixers** will be slightly different, given their definition of 1dB compression point:

$$\begin{aligned} P_{in}^{sat}(dBm) &= P_m^{1dB}(dBm) - G_{m-1}(dB) - G_{m-2}(dB) - \dots - G_1(dB) \\ &= P_m^{1dB}(dBm) - \sum_{n=1}^{m-1} G_n(dB) \quad (\text{for mixers}) \end{aligned}$$

m=5: IF Filter

As we determined earlier, the compression point of a **filter** is effectively **infinity**, and so for this device:

$$P_{in}^{sat} = \infty$$

So, let's **summarize** in our table what we have found:

Device	G_m	P_m^{1dB}	P_{in}^{sat}
m=1	10 dB	+10 dBm	0 dBm
m=2	-1.0 dB	∞	∞
m=3	-6.0 dB	3 dBm	-6 dBm
m=4	15 dB	+14 dBm	-4 dBm
m=5	-2 dB	∞	∞

Q: Wait a second! We have determined four different answers for the receiver input power that will saturate our receiver. Can they all be correct?

A: Absolutely not! There is one, and only one, answer for receiver saturation point P_{in}^{sat} .

→ The receiver saturation point is the smallest of all of our calculated values P_{in}^{sat} !

Thus, for this example, the receiver compression point is:

$$P_{in}^{sat} = -6 \text{ dBm}$$

Q: Why do we consider the smallest of all the values P_{in}^{sat} as the receiver compression point? Why not the largest? Why not the average?

A: A receiver is considered saturated when any of its components are in saturation. Remember, saturation causes our signal to distort, and thus it may not be accurately demodulated. As a result, an input signal power that causes the saturation of even one receiver component is unacceptable.

Thus, by choosing the **smallest** of the input saturation powers, we have selected a value that will **unambiguously** define the point where **even one** component is saturated—if the receiver input power is **less** than even the smallest of our calculated P_{in}^{sat} , then **none** of the receiver components will be saturated.

Q: *In this example, it is the mixer that saturates first. Is this always the case?*

A: It is indeed **often** the case that the mixer is the device that determines the receiver saturation point. However, the **LNA** can likewise be the component that saturates first.

Q: *What can we do to improve (i.e., increase) the saturation point of a receiver?*

A: Considering the discussion of this handout, it should be quite **evident** how to accomplish this.

We can do **two** different things:

1. *Find a **different** component part with a **higher** saturation point P_m^{1dB}*

This strategy at first seems **very simple**. However, a component designer of mixers or amplifiers is faced with the same **design conflicts** and trade-offs that typically face all other design engineers. If he or she **improves** the 1dB compression point, it will undoubtedly **mess-up** some other

important parameter like gain, or bandwidth, or noise figure, or conversion loss.

Thus, a **receiver designer** that attempts to replace a mixer or amplifier with another exhibiting a **higher 1dB compression point** will almost certainly cause some **degradation** in some other receiver performance parameter, like gain, or noise figure, or bandwidth.

→ The selection of receiver component parts is typically a **compromise** between competing and conflicting component parameters. You will **never** find a "perfect" microwave component, only a component which **best suits** the receiver specifications and design goals.

2. Decrease the gain (increase the attenuation) of the component parts preceding the component that saturates.

Decreasing the gain and or increasing the loss of components in a receiver **will** generally improve (i.e, increase) the receiver saturation point. However, it will also **mess-up** the receiver **noise figure** and **MDS**!

→ Again, we are faced with a design trade-off!

Note however, that we only need to decrease the total gain of the components **preceding** the device that is saturating. Another way to accomplish this is simply to **rearrange** the order of the devices in the receiver chain.

For example, we might move an amplifier from a location preceding the saturating component, to a location after the saturating component—this of course reduces the gain of the components preceding the device, but does not alter the overall receiver gain!

Likewise, we might move a lossy component from a location after a saturating component, to a location preceding the saturating component—this again reduces the gain of the components preceding the device, but again does not alter the overall receiver gain!

Thus, we can conclude that the compression point of a receiver will typically improve if we move lossy components to the front and amplifiers to the back!

However, we must keep in mind two things:

- * The order of some devices cannot be changed. For example, we cannot put the mixer before the preselector filter!
- * Although rearranging the order of the components in a receiver will not change the receiver gain, it can play havoc with receiver noise figure and MDS!

In fact, it should be evident to you that the receiver noise figure typically improves if we move lossy components to the back and amplifiers to the front—exactly the opposite strategy for improving receiver saturation!

We find that very often, receiver **saturation point** and receiver **sensitivity** are in direct conflict—improve one and you degrade the other!

